Atomistic Modelisation of Amorphous Materials

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Some common amorphous systems

Usual silicate glasses





Silicates + polymer films

Many polymer glasses ... Amorphous silica in transistors .. Monitor heat transfer, electronic conduction at small scale.



Bulk Metallic Glasses



Preparation

- *) Melt and Quench
- *) Chemical Vapor Deposition
- *) Ion implantation
- *) local melt and quench by laser

General characteristics : (1) Glass transition



General characteristics : (1) Glass transition



General characteristics : Boson Peak



Energy (meV)

0.4

0.5

Generation of amorphous systems from a computer

Amorphous system : lack of long range order (like in a liquid)



Order of magnitude for experimental cooling rates of the order of 1 K/s

Need to obtain representative defect ratios

Difficult task especially if electronic degrees of freedom are included

Use classical potentials to obtain the structure ... still quench.rates are ~10¹⁰ K/s !!!

Some examples of classical potentials :

- B.K.S. : Potential for silica, long range part is numerically heavy Improved version for amorphous systems can include cut-off in the electrostaticinteractions. (A.Carré et al. J. Chem Phys 127 114512 (2007))
- S.W.: Potential for a-Si. Can be modified to tune properties like the nature of the defects and their numbers, DOS,...
- Tersoff : High melting temperature, liquid remains undercoordinated respect to experiments, some weird mechanical properties
- L.J. : Need to use several L..J. Parameters (σ and ϵ) to prevent crystal formation

EAM/MEAM : Can be used to model metallic glasses.

Some methods to generate amorphous samples

W..W.W. Continuous random network (covalent 4-fold, silicon like) :

Random initial positions and relaxations (for a-Si again):

Vink et al. J.Non-Cryst.Solids 282, 248(2001) uses the ART technique Guénolé et al. Phys.Rev .B 87 045201 (2013) France-Lanord et al. J.Phys.Condens. Matter 26 055011 (2014)

Melt and Quench for a-Si systems :

Fusco et al. Phys. Rev.E 82 066116(2010) France-Lanord et al. J.Phys.Condens. Matter 26 055011 (2014)

Melt and Quench for SiO2 :

Sarnthein et al. Phys. Rev.B 52 12690 (1995) (all DFT!) Mantisi et al. Eur. Phys. J. B 85 304 (2012)

Validation, Comparison with Experiments :

a-Si, g(r) from melt and quench

A-Si density of states : Various SW models



^aRef. [12]. ^bRef. [13]. ^cRef. [14]. ^dRef. [15]. ^eRef. [16].

Construction of heterostructures :

Using a mask :

Study heattransfer at c-Si / a-Si interface



Combining potentials :

Core shell nanowires

Some properties from MD :

$$D = \int_0^\infty cvv(t) dt$$
$$cvv(t) = \frac{1}{3} < \vec{v}_a(t0) \vec{v}_a(t0+t) >_{a,t0}$$

Self diffusion

Auto correlation of the velocities

$$\lambda_{xy} = \frac{1}{VkT^2} \int_0^\infty \langle j_x(0) j_y(t) \rangle dt$$
$$j_x = d/dt \, \Sigma_a E_a x_a$$

T 7

Thermal conductivity

$$\eta = \frac{V}{kT} \int_{0}^{\infty} \langle \sigma_{xy}(t) \sigma_{xy}(t) \rangle dt \qquad \text{Shear viscosity}$$

$$\sigma_{xy} = \sum_{a} m_{a} \frac{V_{x,a} V_{y,a}}{V} - \sum_{a} \sum_{b>a} \frac{F_{ab,x} r_{ab,y}}{V} \qquad \text{Stress Tensor}$$

Elementary Plastic Events in Sheared Amorphous Solid

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MD SImulations

Annealing at T= 2500 K with the Tersoff potential

 $T \simeq 10 K$ Minimization (damped dynamics) Change potential to SW, SWM1, SWM2 Annealing at 100K (few ps) followed by coordinates and cell minimization (elimination of residual stress)

Tersoff:
$$V_{ij} = f_C(r_{ij}) [a_{ij}f_R(r_{ij}) + b_{ij}f_A(r_{ij})]$$

SW (2body):
$$V_2(r) = A\left(\frac{B}{r^4} - 1\right) \exp\left(\frac{1}{r - rc}\right)$$

SW (3body): $V_3(r_{ij}, r_{ik}) \neq \lambda \exp\left[\frac{\gamma}{(r_{ij} - rc)} + \frac{\gamma}{(r_{ik} - rc)}\right] \left(\cos\left(\theta_{ijk}\right) + \frac{1}{3}\right)^2$

SWM1 : factor 2 on the 3 body term (favours tetrahedral local structure) SWM2: 0.8 energy scale and factor 1.5 on 3 body term (Mousseau version for A-Si) + others "SWM1 like" potentials with different values of λ + different quenching rates (10¹¹ to 10¹⁴ K/s)

Mechanical Deformation :



- •Successive quasi-static shear strain steps, $\delta \epsilon_{xv}$ =0.001, until 30-50% deformation
- •Strain is imposed via the lattice cell parameters in periodic boundary conditions (no walls)
- •Potential energy is minimized through a damped MD at 0K
- •Volume is constant
- •For each configuration a reverse step is calculated

Atomic displacements



Energy Contributions

A-Si, SW potential





Identify Local Plastic Events and define « Plastic Activity »

We have calculate the forward/backward strain steps :

$$c(i)_{ini} = c(i-1)_{ini} + \delta \varepsilon$$

$$c(i)_{rev} = c(i+1)_{ini} - \delta \varepsilon$$

$$\Delta E_{plas} = E_{rev} - E_{ini}$$

Evaluate contributions to the plastic energy coming from local atomic terms :

We construct a local (atomic) positive defined quantity as the norm of the variation of the atomic energy terms :

$$(\Delta E_i)^2 = \sum_j \left[V_2^{ini}(i,j) - V_2^{rev}(i,j) \right]^2 + \sum_{j,k} \left[V_3^{ini}(i,j,k) - V_3^{rev}(i,j,k) \right]^2$$

 $(\Delta E_i)^2$ Is a local "measure" of plastic activity, invariant respect to translations and rotations

It is coarsed grained and written on a 3D grid to find it's attractors and basins. (Methodolgy similar to Bader charges in Quantum Chemistry)

Basins defined by gradient lines



We add some criteria to select Plastic events among the attractors



Attractor examples :

Link with displacement field :



Using this technique, we determine plastic events centers. Compare with : Eshelby quadrupoles localization of coordination defects in the structure

x2000 (d) PE (eV/ 80 60 y (Å) 40 20 60 80 0 x (Å) (b (e) PE (eV/Å³ 80 60 40 y (Å) 20 40 60 80 100120 0 x (Å) (c) х5 PE (eV/Å³ 0.8 80 0.4 60 40 y (Å) 20 40 60 80 100 20 0 x (Å)

Fusco et al PRE 82 06116 (2010)

Calculate size of events

Size of plastic events

The size of the plastic events are evaluated through a fit of the relaxation of the local energy variations at short distances :

 $\Delta E(r) = a \exp(-wr)$ (w gives the size)

 $\lambda = 23$

 $\lambda = 26.25$

35

λ=40

40

average size of plastic events (Angstroms)

6.5

6.0

5.5

5.0

4.5

4.0

3.5

3.0

0

(a)

15

10

20

25

shear strain (%)

30



Plastic events tend to grow in size until the "Yield point"

Plastic energy .vs. local plastic activity

A-Si, SW potential



We have identified localized Plastic Events from atomistic calculations

•To which extend can we compare these results with the elasticity of continuum medium ?

Bridge with mesoscopic models

•Validation, identification of important parameters to describe plastic behaviour

Elements to describe plasticity in an amorphous system :

Continuum mechanics : Elastic field due to a shear inclusion

$$\sigma_{ij} = \frac{a^{3}}{2(1-\nu)R^{3}} \left\{ \frac{p_{ij}}{15} (10(1-2\nu)+6\frac{a^{2}}{R^{2}}) + \frac{p_{ik}x_{k}x_{j} + p_{jk}x_{k}x_{j}}{R^{2}} (2\nu - \frac{a^{2}}{R^{2}}) + \frac{\delta_{ij}p_{kk}}{15} (3\frac{a^{2}}{R^{2}} - 5(1-2\nu)) + \frac{\delta_{ij}p_{kk}x_{k}x_{l}}{R^{2}} (1-2\nu) - \frac{a^{2}}{R^{2}}) - \frac{x_{i}x_{j}p_{kl}x_{k}x_{l}}{R^{4}} (5-7\frac{a^{2}}{R^{2}}) + \frac{x_{i}x_{j}p_{kk}}{R^{2}} (1-\frac{a^{2}}{R^{2}}) \right\}$$





"Shear Transformation Zone"

Argon Acta.Metall. 27 47 1979

Irreversible shear transformation (dozen of particles)

$$u_{i} = \frac{(1+\nu)a^{3}}{2(1-\nu)E} \left\{ \frac{(2p_{ik}x_{k}+p_{kk}x_{i})}{15R^{5}} (3a^{2}-5R^{2}) + \frac{p_{jk}x_{j}x_{k}x_{i}}{R^{7}} (R^{2}-a^{2}) + \frac{4(1-\nu)p_{ik}x_{k}}{3R^{3}} \right\}$$

$$p_{ij} = \frac{E}{(1+\nu)} \{ \epsilon_{ij} + \nu \delta_{ij} \frac{\epsilon_{kk}}{1-2\nu} \}$$

Displacement field has the symmetry Of a field from a magnetic quadrupole



Many mesoscopic models ...

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Free volume theory (Spaepen et al)
Mean Field STZ theory (Falk, et al)
Pinning/Depinning (Vandembroucq et al)
Fluidity models (Picard et al)
KFC-FE models (Schuh et al)
QPD model (Perez et al)
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These models can give : Yield, plastic flow, plastic hardening, shear bands, complex rate dependent behaviour ..

Validation at the microscopic (atomic) scale?

. . .

Pinning /Depinning models : stress(σ) = elastic contrib. ($\mu\gamma$) + stress from Local event G(x,y,x',y')

J.C. Baret et al. Eshelby-like stress redistribution upon event PRL 89 195506 (2002) Local (random) stress threshold

Fluidity models : $\dot{\sigma}(z)$

$$\dot{\sigma}(x, y, t) = \mu \dot{\gamma} + 2\mu \int G(x', y', x, y) \varepsilon^{pl}(x', y')$$

G.Picard et al PRE 71 010501 (2005)

Eshelby-like stress redistribution upon event Fixed stress threshold $\dot{\epsilon}^{pl}(x, y, t) = \frac{n(x, y, t)}{2\mu\tau}\sigma(x, y, t)$

n(x,y,t) depends on characteristic times when it switches from elastic (n=0) to plastic (n=1) or vice-versa.

KMC-FE models :Define STZs on a FE grid
Use an activation rates that depends on
Typical STZ barrier and local stress : $\dot{s} = v_0 \exp(\frac{-\Delta F + \tau \gamma_0 \Omega_0}{kT})$ Acta Mater. 57 2823 (2009)

Eshelby-like stress redistribution upon event

Fitting displacements with Eshelby inclusions

Least square fit from the difference of MD displacements and a sum of Eshelby inclusions centered on detected plastic events

Variational parameters : Transformation strain tensor (6 components)

Other parameters : inclusion radius, average elastic constants

Rules : use homogeneous infinite body solutions, Spherical inclusions do not fit regions inside inclusions Use events that represent more than 90% of plastic activity

Technique : Damped dynamics algorithm

Results on events extracted from the simulation and studied alone using a small rescaling factor : ...



•Symmetry and power law correspond to shear Eshelby event

Nature of the plastic events



•Events centers do correspond to detected plastic events

- •Shear inclusions describe well the overall structure of the displacement field with characteristic cross shaped structures.
- •Max. errors are found close to the centers

Typical errors & symmetry

Rsym : ratio between (sum of displacements square due to diagonal components of ϵ^{T}) and (sum of displacements square due to shear components of ϵ^{T})

Rprec : ratio between (final objective function) and (initial objective function)



Distributions of Eshelby Transformation Tensors



 ϵ V represents the robust output of the fit

Stress-Strain relations evaluated from the Eshelby shear inclusions



•Homogeneous strain correction to match BC

•1 adjustable parameter α

Stress-Strain relations evaluated from the Eshelby shear inclusions



•Continuum elastic solutions of shear inclusions describe well the development of plasticity

- •... providing we evaluate their intensity and number, and the use of a variableG
- •Variable poisson parameter and precise Eshelby radius are not crucial
- •No need of diagonal components to represent shear stress
- •What is the origin of the parameter α close to 2 ?

Local Contributions ::



Volume and pressure Variations

Diagonal elements of Eshelbv transformation strain tensors :



Volume decrease around SW plastic event Volume increase around SWM plastic event Large variations at band formation ???

Consistent with atomistic structure around plastic event :



- Explained by 3 body param
- •Linked to relative brittle/ductile behaviour of SW and SWM
- •Hard sphere plasticity fails at atomic scale
- Inclusion model quantitative respect to pressure ?

Volume and pressure Variations



Inclusion mode lis no more accurate $\delta P = \delta P^{el} + \alpha \delta P^{plas}$

Reasons : elastic term more difficult to evaluate Many sets of inclusions give similar accuracy, especially with lot of inclusions Large jumps are due to numerical artefact

Adding pressure in the fit :



Conclusions and Perspectives

•Main features of plasticity can be described through Eshelby inclusion representation

•Allow better comparison between exp./theory.

•Important parameter here is mainly the average shear modulus, for a sheared bulk the size of events and their shapes are not crucial

•Small scale details determine the occurrence of events but once they are generated these events are well described by continuum medium elasticity.

•Boundary conditions matter but can be discussed even using a simple infinite elastic body solutions. For any quantitative model they largely affect the results and should be considered.